MDOT Camelback Bridge Example

AASHTOWare Bridge Rating

May 2022

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This tutorial was created on behalf of MDOT by the Center for Technology & Training, please contact <u>loadrating@mtu.edu</u> for assistance or visit <u>http://loadrating.michiganltap.org/</u> for more information.





Background

What follows is a general guide for modeling a camelback bridge in AASHTOWare Bridge Rating (BR). The sample bridge was taken from a set of MDOT standard plans for a 60-ft reinforced concrete girder with a 22-ft roadway. A similar approach can be applied to other standard lengths. The tutorial methodology should be adapted accordingly for any modifications to the standard plan and for the specific rebar present in the bridge.

This tutorial is being provided by the Michigan Department of Transportation (herein referred to as MDOT) as a courtesy service to contractors, consultants and local agency bridge owners. In preparation of this tutorial, MDOT has endeavored to offer current, correct and clearly expressed information. However, error may occur. MDOT expressly disclaims any liability, of any kind, for any reason, that might arise out of the use of this tutorial.

Assumptions/Limitations

This tutorial is prepared based on the assumption that the bridge is in a pristine, un-deteriorated state and was built in accordance with the construction plans. All load ratings must reflect the current condition of the structure. The load rating engineer should perform a field evaluation to confirm the correctness of the plans and use engineering judgment to determine whether any observed deterioration may affect the structural capacity of the bridge.

In a more traditional girder arrangement the compression zone of each girder is laterally braced by the bridge deck. The camelback bridge design results in an un-braced compression zone. This situation is not addressed by AASHTOWare Bridge Rating. Should there be evidence of distress in the compression zone of a camelback beam; a more detailed finite element model may be warranted.

The deck is conservatively considered for weight only, and contributes no structural capacity to the bridge as modeled in this tutorial. For situations where additional capacity is needed in the bridge, a portion of the deck slab can be considered as a structural part of the girder, subject to the limitations of AASHTO Section 8. Note that BR calculates the weight of the structural portion of the deck, so it should be deducted from the additional self-load entered on the Member Alternative Description screen.

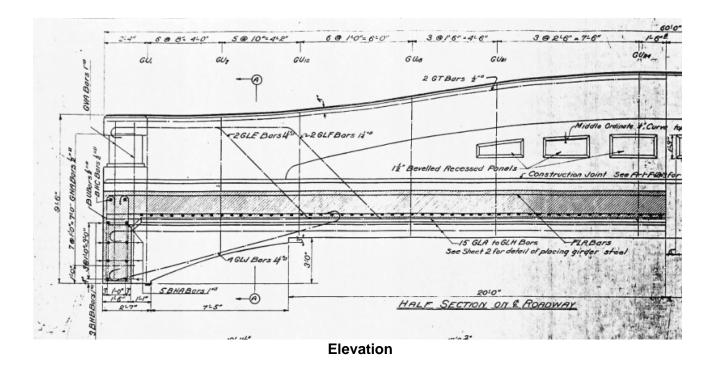
Material properties have been assumed, according to the age of the bridge, using the Michigan Bridge Analysis Guide (BAG). The most recent bridge design revision date from the standard plans was 1922, which was assumed to coincide with construction for the purpose of determining material properties.

BAG, Table 10.28: 1922-1935 Grade A Concrete: f'c = 3 ksi Es/Ec = n = 12

BAG, Table 10.26: Structural or unknown grade prior to 1954: fy = 33 ksi







General Bridge Information

From BR's Bridge Explorer window, create a new bridge by selecting *File/New/New Bridge* and enter the following description data:





| A | New | Brid | qe |
|----------|--------|------|-----|
| **** | 1 ACAA | DITU | чyс |

| _ | × |
|---|---|
| | |

| | | Template | Superstructures |
|---------------------------|--|---------------------------------|-------------------------------------|
| Bridge ID: Camelback | NBI structure ID (8): Camelback | Bridge completely defined | Culverts |
| | | | Substructures |
| Description Description (| (cont'd) Alternatives Global reference poin | It Traffic Custom agency fields | |
| Name: Sample | e of a Camelback Bridge Load Rating | Year built: 1922 | |
| | on MDOT standard plans for a 60-ft reinforced c with a 22 ft roadway. | oncrete camelback | |
| Location: Michig | gan | Length: 60.00 | ft |
| Facility carried (7): | | Route number: 01 | |
| Feat. intersected (6): | | Mi. post: | |
| Default units: US Cus | stomary 🗸 | | |
| | | | |
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| | | | |
| AASHTOWare association. | BrR ØBrD BrM | | |
| | | | |

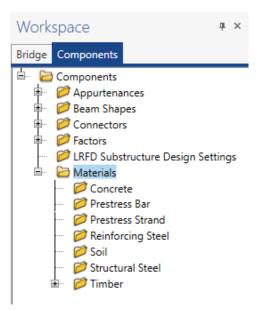
Close the window by clicking **OK**. This saves the data to memory and closes the window.





Material Properties

Enter the materials to be used by members of the bridge by clicking on + to expand the tree for Materials, listed under the Components tab in the Workspace window. The tree with the expanded Materials branch is shown below:



To add a new concrete material click on **Concrete** in the tree and select *File/New* from the menu (or right mouse click on **Concrete** and select *New*).

Enter the data shown in the window below.





🕰 Bridge Materials - Concrete

| Name: | Concrete-1922 | | |
|----------------|----------------------------|--------------|-----|
| Description: | Estimated from the BAG | table 10.28 | |
| Compressive | strength at 28 days (f'c): | 3.000 | ksi |
| Initial compre | essive strength (f'ci): | | ksi |
| Composition | of concrete: | Normal |] |
| Density (for o | dead loads): | 0.150 | kcf |
| Density (for r | modulus of elasticity): | 0.150 | kcf |
| Poisson's rati | 0: | 0.200 | |
| Coefficient of | f thermal expansion (α): | 0.0000060000 | 1/F |
| Splitting tens | ile strength (fct): | | ksi |
| | Compute | | |
| Std modulus | of elasticity (Ec): | 3320.56 | ksi |
| LRFD modulu | us of elasticity (Ec): | 3879.84 | ksi |
| Std initial mo | dulus of elasticity: | 0.00 | ksi |
| LRFD initial n | nodulus of elasticity: | 0.00 | ksi |
| Modulus of r | upture: | 0.416 | ksi |
| Shear factor: | | 1.000 | |

| Copy to library | Copy from library | OK | Apply | Cancel |
|-----------------|-------------------|----|-------|--------|
| | | | | |

Click **OK** to save the data to memory and close the window.

Double click on **Reinforcing Steel** in the bridge tree. The reinforcing steel may be copied from the library. Select the **Copy from Library...** button and choose the appropriate material from the list. The window will look like that shown below:





– 🗆 🗙

🕰 Bridge Materials - Reinforcing Steel

| _ | \times |
|---|----------|
| | |

| Name: | Structural or u | nknown grade prior | | | | |
|----------------------------------|-------------------|----------------------|--------------|----|-------|--------|
| Description: | Structural or u | nknown grade prior t | o 1954 | | | |
| Material prop | perties | | | | | |
| Specified yiel | ld strength (fy): | 33.000 | ksi | | | |
| Modulus of e | elasticity (Es): | 29000.00 | ksi | | | |
| Ultimate strength (Fu): 60.000 | | ksi | | | | |
| Type Plain Epoxy Galvan | ized | | | | | |
| | Copy t | co library Copy | from library | ОК | Apply | Cancel |

Click **OK** to save the data to memory and close the window.





Superstructure Definition

The default impact factors will be used so we can skip to **Structure Definition**, listed under the Bridge tab in the Workspace window.

| 🚯 Bridge Workspace - Camelback | |
|-------------------------------------|--|
| 🖃 🕰 Camelback | |
| 🗄 📖 🧰 Materials | |
| 🧰 Structural Steel | |
| 🚊 📖 🧰 Concrete | |
| 🛄 🚺 Concrete-1922 | |
| 🖕 🧰 Reinforcing Steel | |
| Unknown grade prior 1954 | |
| 🚞 Prestress Strand | |
| 📄 Prestress Bar | |
| 🗄 🚥 Timber | |
| L 📄 Soil | |
| 🗄 ····· 🧰 Beam Shapes | |
| 🗄 ····· 🧰 Appurtenances | |
| 🚞 Diaphragm Definitions | |
| 📖 Lateral Bracing Definitions | |
| Impact / Dynamic Load Allowance | |
| MPF LRFD Multiple Presence Factors | |
| 🗄 ····· 🧰 Factors | |
| 🔤 LRFD Substructure Design Settings | |
| EC Environmental Conditions | |
| Design Parameters | |
| DEFINITIONS | |
| 🛄 BRIDGE ALTERNATIVES | |
| | |
| | |

Doubleclick on **SUPERSTRUCTURE DEFINITIONS** to create a new structure definition. The following dialog will open.





| A | New | Su | perstructure Definition | ۱. |
|----------|-----|----|-------------------------|----|
|----------|-----|----|-------------------------|----|

| Girder system superstructure | |
|---|----------------------------------|
| Girder line superstructure | Superstructure definition wizard |
| Floor system superstructure | |
| Floor line superstructure | |
| Truss system superstructure | |
| Truss line superstructure | |
| Reinforced concrete slab system superstructure | |
| Concrete multi-cell box superstructure | |
| | |
| | |
| | |
| | |
| | |
| | |
| | |

OK

Cancel

Select **Girder System Superstructure** and the Structure Definition window will open. Enter the data shown below:

Click **OK** to save the data to memory and close the window.





🕰 Girder System Superstructure Definition

| _ | П | × |
|---|---|---|
| | | ~ |

| Definition Analysis Specs | Engine | | | |
|---|---|--------|-----|---|
| Name: Camelback | | | | Frame structure simplified definition |
| | | | | Deck type: |
| Description: | | | | Concrete Deck |
| Default units: US Customary Number of spans: 1 💭 Number of girders: 2 💭 | Enter span lengths along the reference line: Span Length (ft) 1 60.00 | | | For PS only Average humidity: % Member alt. types Steel P/S R/C Timber |
| Horizontal curvature along refere | | | | |
| Horizontal curvature | Distance from PC to first support line: | | ft | |
| Superstructure alignment | Start tangent length: | | ft | |
| Curved | Radius: | | ft | |
| ◯ Tangent, curved, tangent | Direction: | Left v | n. | |
| Tangent, curved | | Len v | ft | |
| Curved, tangent | End tangent length: | | ft | |
| | Distance from last support line to PT: | | | |
| | Design speed: | | mph | |
| | Superelevation: | | % | |
| | | | | |

OK Apply

Cancel



Load Case Descriptions

Click **Load Case Description** in the bridge tree by expanding the Superstructure Definition branch to define the dead load cases. Select **Add Default Load Case Descriptions**. The completed Load Case Description window is shown below.

| Load case name | Description | Stage | | Туре | Time* (days) | | |
|----------------|-------------|-------|------|------|-----------------|--|--|
| DC1 | DC acting | N * | D,DC | Ŧ | | | |
| DC2 | DC acting | C * | D,DC | - | | | |
| DW | DW acting | C * | D,DW | - | | | |
| SIP Forms | Weight du | N * | D,DC | - | | | |
| | | | | | | | |
| | | | | | | | |

Click **OK** to save the data to memory and close the window.





Framing Plan Details

Double-click **Framing Plan Detail** in the tree to describe the framing plan. Enter the data shown below.

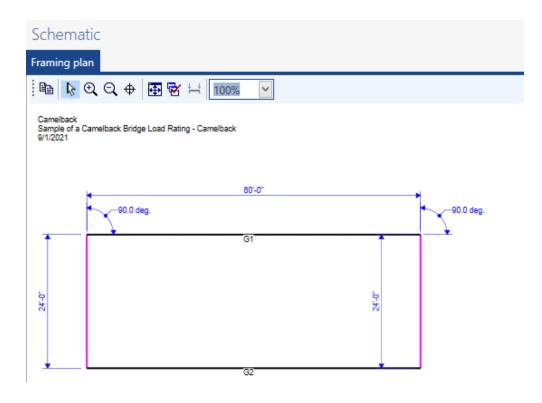
| ayout Diaphragms | | |
|------------------------|---|--|
| Support Skew (degrees) | Girder spacing orientation Perpendicular to girder Along support | |
| 2 0.000 | Girder Girder spacing (ft) Start of girder End of girder 1 24.00 | |

Select **OK** to close the window.

It is always a good idea to check the schematic after entering the framing plan detail information. Do this by selecting the **schematic** button while **framing plan detail** is highlighted in the bridge workspace tree. Alternatively, you may select *Bridge/schematic* while the **framing plan detail** is highlighted.







Typical Section

Next define the structure typical section by double-clicking **Structure Typical Section** in the Bridge Workspace tree. Input the data describing the typical section as shown below.





Deck Geometry

| ۵ | Structure Typical Section | |
|---|---|--|
| | Distance from left edge of deck to superstructure definition ref. line | Distance from right edge of deck to superstructure definition ref. line |
| | Γ, · · · · | Superstructure Definition |

| | Deck thickne | BSS | Superstruct Reference I | ure De Line | efinition | 4 | | | | | | |
|------------------|---|---------|----------------------------|----------------|-----------|--------|---------|---------------|---------------|-----------------|-------|--------|
| Left overhang | 4 | | | | | , F | light a | verhang | | | | |
| Deck Deck (co | ont'd) Parapet | Media | n Railing | Ge | eneric | Sidew | alk | Lane position | Striped lanes | Wearing surface | | |
| Superstructure d | efinition reference | line is | within | | ✓ the | bridge | deck. | | | | | |
| | | | Start | | En | d | | | | | | |
| | t edge of deck to efinition reference | line: | 13.00 | ft | 13.00 | | ft | | | | | |
| | ht edge of deck to efinition reference | | 13.00 | ft | 13.00 | | ft | | | | | |
| Left overhang: | | [| 1.00 | ft | 1.00 | | ft | | | | | |
| Computed right | overhang: | | 1.00 | ft | 1.00 | | ft | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | OK | Apply | Cancel |

The **Deck (cont'd)** tab is used to enter information about the deck concrete and thickness. The material to be used for the deck concrete is selected from the list of bridge materials described in the Background section.





_

A Structure Typical Section

| Distance from left edge superstructure definition | e of deck to j Distance from right edge of deck to n ref. line superstructure definition ref. line |
|--|---|
| De | ick 4 Superstructure Definition 7 skress I Reference Line 7 |
| | |
| Left overhang | Right overhang |
| Deck Deck (cont'd) Parap | et Median Railing Generic Sidewalk Lane position Striped lanes Wearing surface |
| Deck concrete: | Concrete-1922 |
| Total deck thickness: | 18.0000 in |
| Load case: | Engine Assigned |
| Deck crack control parameter: | kip/in |
| Sustained modular ratio factor: | 3.000 |
| Deck exposure factor: | |
| | |
| | |
| | |
| | |
| | |
| | |
| | |
| | |
| | OK Apply Cancel |

_





Lane Positions

Select the Lane Position tab. Manually enter the width of the travelway as shown in the figure below

| ruc | ture Typical S | Section | | | | _ | |
|-----|---------------------|--|---|--|---|------|--------|
| | Travelw | | ravelway 2 | | | | |
| ck | Deck (co | nt'd) Parapet Median | Railing Generic Sidewa | alk Lane position Striped | l lanes Wearing surface | | |
| | Travelway number | Distance from left edge of travelway to superstructure definition reference line at start (A) (ft) | Distance from right edge of travelway to superstructure definition reference line at start (B) (ft) | Distance from left edge of travelway to superstructure definition reference line at end (A) (ft) | Distance from right edge of travelway to superstructure definition reference line at end (B) (ft) | | |
| Þ | 1 | -11.00 | 11.00 | -11.00 | 11 | | |
| | | | | | | | |
| | | ilable to trucks: | Compute | | New Dupli | cate | Delete |
| | | | | | | | |

Click **OK** to save the data to memory and close the window.

It is also a good idea to check the schematic after entering the structure typical section information. This is done in the same manner as was used to check the schematic of the framing plan details. Note that for reinforced concrete structures a generic beam shape is used to represent the beam.





| chematic | | |
|---|--------------------------------|-----------|
| raming plan Typi | cal section | |
| 🖻 <u>र</u> 🔍 🔍 | 0% 🕂 🔂 | |
| Camelback Sample of a Ca 9/1/2021 | melback Bridge Load Rating - C | Camelback |
| • | 26'-0" | |
| | 22'-0" | |
| Decl | Thickness 1'-6" | |
| 1 | Travelway 1 | |
| | | |
| 1' 0" | 24'-0" | 1"-0" |

Shear Reinforcement

Now define the vertical shear reinforcement by double-clicking on **Vertical** (under **Shear Reinforcement Definitions** in the tree). Define the reinforcement as shown below.

| cal | | | _ | |
|----------------------|---|---|--|--|
| | | | | |
|] | | | | |
| Material: | Structural or | unknown grade prio | r | > |
| Bar size: | 7 🗸 | | | |
| Number of legs: | 2.00 |] | | |
| Inclination (alpha): | 90.0 | Degrees | | |
| nt | | | | |
| | | | | |
| | | | | |
| | | | | |
| | Material: Bar size: Number of legs: Inclination (alpha): | Material: Structural or Bar size: 7 Number of legs: 2.00 Inclination (alpha): 90.0 | Material: Structural or unknown grade prior Bar size: 7 Number of legs: 2.00 Inclination (alpha): 90.0 | Material: Structural or unknown grade prior Bar size: 7 Number of legs: 2.00 Inclination (alpha): 90.0 |

Click **OK** to save to memory and close the window.





Cancel

OK

Apply

Member Descriptions

The Member window shows the data that was generated when the structure definition was created. No changes are required at this time. The first Member Alternative that we create will automatically be assigned as the Existing and Current Member alternative for this member (as shown below).

| A Member | _ | | × |
|--|-------------------|------|-----|
| Member name: G1 Link with: None | Link with: None 🗸 | | |
| Description: | | | |
| Existing Current Member alternative name Description | | | |
| | | | ^ |
| | | | |
| | | | |
| | | | - |
| span length | | | |
| | | | |
| | | | |
| | | | |
| | | | |
| OK | Apply | Cano | el: |

Double-click **MEMBER ALTERNATIVES** in the tree to create a new alternative. The New Member Alternative dialog shown below will open. Select **Reinforced Concrete** for the Material Type and **Reinforced Concrete I** for the Girder Type.

| 🗛 New Member Alternative | × |
|-------------------------------------|-------------------------|
| Material type: | Girder type: |
| Prestressed (pretensioned) concrete | Reinforced Concrete I |
| Reinforced concrete | Reinforced Concrete Tee |
| Steel | |
| Timber | |
| | |
| | |
| | OK Cancel |

Click **OK** to close the dialog and create a new member alternative.





The Member Alternative Description window will open. Enter the appropriate data as shown below. Note: BR 6.4.1 will not automatically calculate and include the self-weight of the deck. Therefore, you must estimate the weight of the deck and apply it to the beam as an additional self-load. In this example, the deck is 1.5 feet thick and spans 22 feet between beams. Therefore, the additional self-load can be approximated as 11 ft*1.5 ft*0.150 k/ft³ = 2.475 k/ft, which is entered below.

By entering the deck weight at this location you are assuming that the deck and slabs were cast as a single unit while supported by false work. If this condition does not appear to be true for your particular bridge you should instead add the deck weight as an additional uniform load under the **Member Loads** tab.

| and cr arcenta | tive: Car | nelback bea | m | | | | | | |
|----------------|------------|-------------|--------|-------------|------------------|------------------|-----------|--|--|
| Description | Specs | Factors | Engine | Import | Control options | | | | |
| Description: | | | | | Material typ | e: Reinforced Co | oncrete | | |
| | | | | | Girder type: | Reinforced Co | oncrete l | | |
| | | | | | Default unit | : US Customan | у 🗸 | | |
| Girder pro | perty inpu | it method | End be | aring locat | ions | | | | |
| ⊖ Schedu | | | Left: | | in | | | | |
| Cross-s | ection bas | sed | Right: | | in | | | | |
| Self load | | | | | Default rating m | athod | | | |
| Load case: | | Engine Ass | ianed | ~ | LFD | ~ | | | |
| Additional | self load: | | kip/ft | | | | | | |
| Additional | | | % | | | | | | |
| | | | | | | | | | |
| Crack cont | | eter (Z) | 1 | Exposure | | | | | |
| Bottom of | beam: | | kip/in | Bottom of | of beam: | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
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| | | | | | | | | | |





Expand **Member Alternatives** and **camelback beam (E)(C)** portions of the tree. The default materials for the member alternative must be defined. Enter data as shown in the figure below.

| 🕰 Default Materials | | | _ | × |
|------------------------|-----------------------------------|--------------|---|---|
| Member alternative nam | e: Camelback beam | | | |
| Deck concrete: | Concrete-1922 | ~ | | |
| Deck reinforcement: | Structural or unknown grade prior | ~ | | |
| Beam concrete: | Concrete-1922 | \checkmark | | |
| Reinforcement: | Structural or unknown grade prior | ~ | | |
| Stirrups: | Structural or unknown grade prior | ~ | | |

| OK | Apply | Cancel |
|----|-------|--------|
|----|-------|--------|





Open the Live Load Distribution window from the tree beneath camelback beam.

| | actor inp | ut method | | | |
|-----------------|------------|-------------------|-------------------|----------------|---|
| Use simpli | fied met | nod 🔾 | Use advanc | ed method | ○ Use advanced method with 1994 guide specs |
| Allow distrib | oution fac | tors to be u | used to com | pute effects (| of permit loads with routine traffic |
| | | | ution factor | | |
| Lanes Ioaded | Shear | Shear at | /heels) Moment | Deflection | |
| 1 Lane | 1.500 | supports 1.500 | 1.500 | 1.000 | |
| Multi-lane | 2.083 | 2.083 | 2.083 | 2.000 | |
| | | | | | |
| | | | | | |

If we try to use the **Compute from Typical Section** button on the Live Load Distribution **Standard tab** to populate the LFD live load distribution factors for this member alternative, we will receive a message that BR cannot calculate the distribution factors because beam shapes are not assigned to adjacent member alternatives.

You must revisit this window after the member alternative has been created for the other side of the bridge. Then the **Compute from Typical Section** button will compute the distribution factors for you.

Cross Sections

The camelback shape will be modeled as a series of cross sections located at discrete points. Cross sections should be determined for 10th points along the length of the bridge. An elevation of half the bridge and half

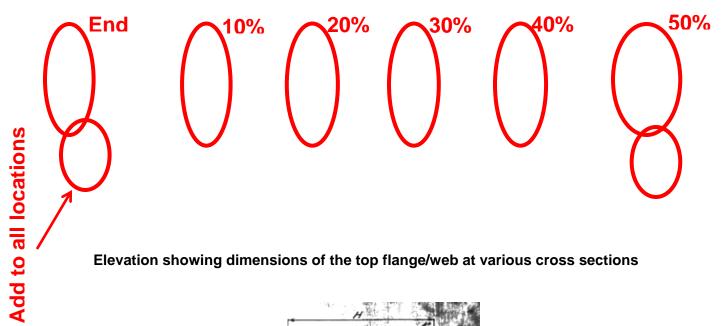




sections for the end and center of the bridge are shown below along with a rebar schedule for interpretation of the reinforcing steel identified in the half sections. The cross section can be modeled as an I-beam. Use the elevation to determine the flange and web heights and the half section to determine the flange and web width and the rebar placement. If the section contains square reinforcing bars substitute those with the largest modern rebar size that produces an equal or lesser cross sectional area. In this example; No. 11 rebar (1.56 in²) was used to represent 1.25-in square rebar (1.56-in²). Additional rebar could be added to bring the total cross sectional area of steel in the model to what is found in the bridge provided no deterioration has occurred. Pay careful attention to any changes in rebar placement at the different cross sections. Steel reinforcing plans and elevations along with bending diagrams have been shown to provide the necessary information to ensure proper rebar locating at each section.





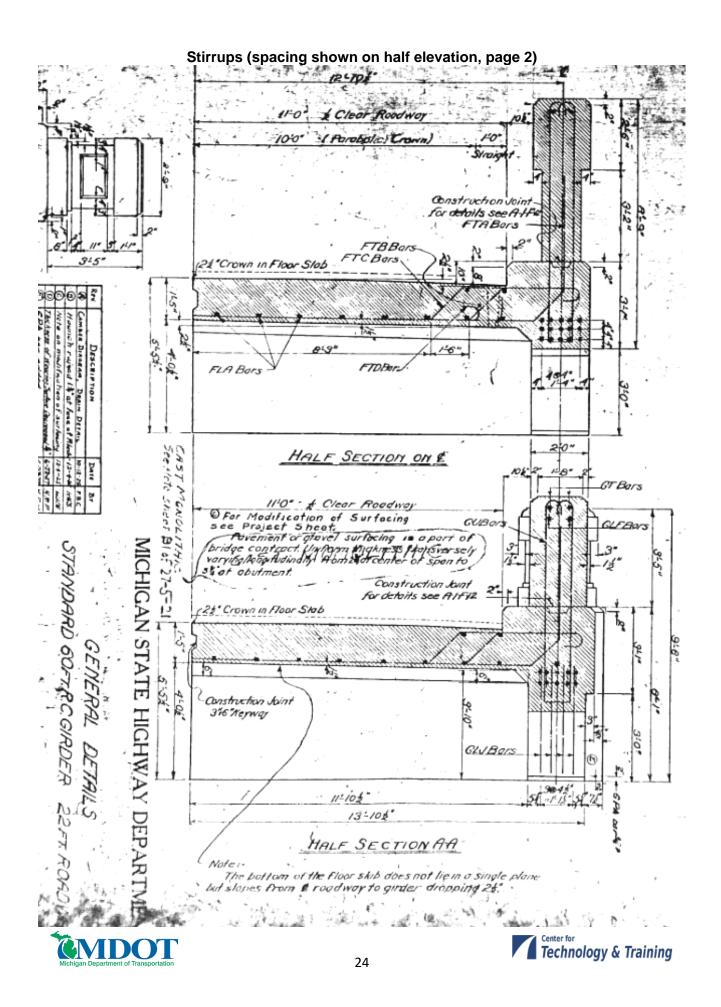


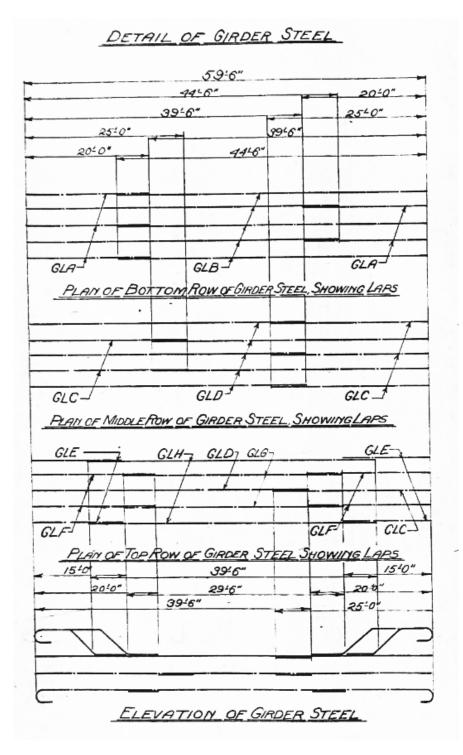
Elevation showing dimensions of the top flange/web at various cross sections

| | | W a | H | 47 | | Č. |
|-----|--------|------|-------|------------------|--------|------|
| | - | | | and and a second | E. | 1.11 |
| ٠f | | | 11 | | Dig | 8 |
| •0/ | | | 4 | 4 | 10 | |
| T | | | 10 | shi. | S SPAR | 2 |
| | GU, to | o Gu | y Bo | 13 2 | 10 3 | 8 |
| | Mork | No. | | Length | Weight | £. |
| | GU, | 4 | 8-7" | | 161 - | 3 |
| | " 2 - | 4 | 8.4" | | 159 | |
| | " 3 | 4 | 8:2" | 19:2 | 157 | 24 |
| | 1.4 | 4 | 7:11" | 18:8 | 153 | 13 |
| | + 5 | 4 | 78 | 18:2" | 149 | 3 |
| | ~ 6 | 4 | 7:6 | 17:10 | 146 | 驗 |
| | 7 | 9 | 7:3 | 17-4 | 192 | 52 |
| | -8 | 1 | 7-1" | 17:00 | 139 | 1 |
| | وم | 1 | 6:10 | 16:6 | 135 | ÷4 |
| | "10 | 1 | 6: 7 | 16:0" | 131 | 52 |
| | · // | 9 | 6:5" | 15-8- | 128 | ÷. |
| | -12 | 1 | 6-3 | 15:4 | 125 | |
| | -13 | 4 | 6-3 | 15-4 | 125 | Č. |
| | - 14 | 4 | C:5* | 15:8 | 128 . | ЧĘ., |
| | -15 | 9 | 6:6" | 15:10 | 129 | ς. |
| | -14 | 4 | 648 | 1612 | 132 | - |
| | * /Z | 4 | 6-10 | 16:6 | 135 | ÷ |
| | + /A | 4 | 7-0 | 16:10 | 138 " | ÷ |
| | | 1 | 7-3 | 17-4" | 142 | γ. |
| | ~20 | 4 | 7-6" | 1740 | 146 | |
| | .21 | 4 | 7'8 | 18:2" | 149 | |
| | 122 | 4 | | 18'6 | 151 . | |
| | | 4 | | 19:00 | 155 | h, |
| | "24 | 1 | 8:2 | 1912 | 157 |) |
| | Total | | 1 | | 34154 | Ċ. |
| | | | | | | |









Longitudinal Steel Placement

Note: From the elevation we see that the rebar in the third row from the bottom changes depth over the length of the bridge. The two outer bars (GLE) are located higher in the section and then drop down, followed by the

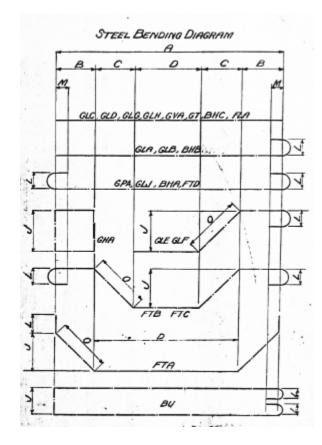




two inner bars (GLF). The center bar (GLC/CLD) remains at the same location over the length. This has been reflected in the cross sections modeled in BR (details on the next page).

| | 1.1.1 | | | 5 | TLL | 01 | O/L | | DAA | 1.00 | ň 🖓 | 電音 | | |
|----------|-------|-------|-------|------------|-------|-------|------|------|--------|------|-------|-----------------------------------|----------|--------|
| LOGATION | MARK | A | В | C | D | L | J | M | 01 | No | Sie | Kind | Length | Weight |
| GIRDER | GLA | 20'0 | | 31, 1 1 | ° | 75" | 1 | 5" | | 10 | 14% | Der | 2115" | 1138 |
| | GLB | -79'E | | 8 | 1.4.1 | 76 | di | . 5" | · . | 10 | 140 | * | 45:7" | R422 |
| | GLC | 25:0 | | 3.15 | 12 | 24.1 | | | 1.1 | 12 | 140 | · · · · | 25'0" | 1594 |
| | GLD | 39'6' | 1.1 | 8 · · · | 2.1 | 0.5 | - h. | - 2 | | 12 | 140 | | 39-6" | 2518 |
| | GLE | | 4:10" | 4110 | 5:0" | 75" | 440 | 5" | 6110- | 8. | 142 | <u>н</u> | 18:1" | 768 |
| | GLF | | 9:10 | 410 | 5:00 | 26 | 140 | 5" | 6-10- | 8 | 1400 | 20.0 | 23:1" | 98/ |
| | GLG | 29'6 | - 2 | 1.1 | 医肌肉 | 1998 | 1.15 | 1.10 | | | 1400 | $\tilde{\sigma} \rightarrow 0$ | 2946" | 627 |
| | GLH | 39.6 | 1.1 | 1162 | 6754 | · 98字 | 5 | 13 | 医囊儿 | 12 | 14 40 | 1. | 39:6" | 839 |
| | GLU | 12:9 | 181 | 662 | 18-3 | 76 | 6438 | 5 | 医复合管 | 76 | 1400 | 신원 # ` | 15:7" | 1324 |
| | GT | 320 | 1.54 | 2.2 | 87.3 | 10.14 | 14 | 180 | (1, 1) | 184 | 6.ª# | $\sim r_{e^{-1}}$ | 32'0" | 218 |
| | GU 3 | See | Tel | offe | WB. | 13 | 1010 | 54 | 16.00 | 法罪 | 6.57 | 件人 | | 3,415 |
| | GHA | | 1-10 | S^{*} | 6 | 100 | 1.7% | | 1.12 | 32 | 10 | | 6 6- 11" | 188 |
| | GVA | 90 | 1.1 | 1.78 | 8 | 3.861 | 1.2 | 12 | 545 | 10 | 100 | $\mathcal{S}_{1,\mathcal{O}_{1}}$ | 940- | 490 |
| | | | | | | | | | | | | | | |

| | 1. L. A. J | 1.128 | 4. ⁴¹² a | | |
|-----|------------|-------|---------------------|--|--|
| BIL | LOF STEEL | BARS | 1.50 | | |



Description and Bending Details of Longitudinal Girder Reinforcing Steel





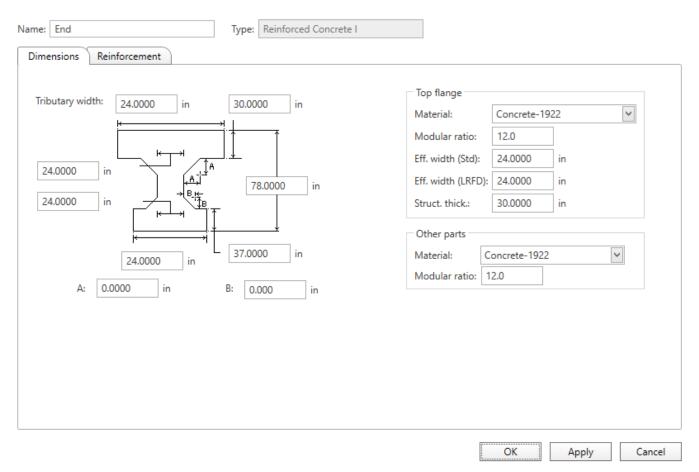
Cross Section Locations:

End - GLE and GLF both up 4'-10" from the 3rd row (70" from bottom of beam) 10% - GLE @ 3'-8" from the 3rd row (56" from bottom), GLF @ 4'-10" from 3rd row (70" from bottom) 20% - GLE @ 3rd row (12" from bottom), GLF @ 2'-8" from 3rd row (44" from bottom) 30% - GLE and GLF @ 3rd row (12 inches from bottom of beam)

Next describe the beam by double-clicking on **Cross Sections** in the tree. The Cross Sections windows with the cross sections identified from the plans are shown below. Remember to enter rebar locations as appropriate for the cross section, keeping in mind that these may change over the length of the bridge. In the following cross sections, the #4 rebar at the top of the section was assumed based on scale from the plans.





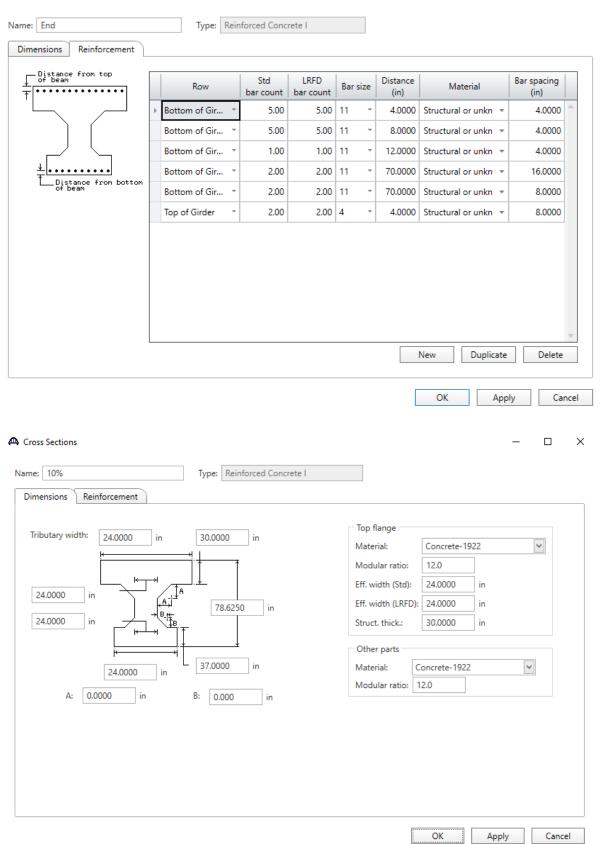






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Technology & Training

| Distance from top of beam | | Row | | Std bar count | LRFD bar count | Bar | size | Distance (in) | Material | Bar spacing (in) | |
|---|---|---------------|---|------------------|-------------------|-----|------|------------------|----------------------|---------------------|---|
| | I | Bottom of Gir | * | 5.00 | 5.00 | 11 | - | 4.0000 | Structural or unkn 🔻 | 4.0000 | ^ |
| | | Bottom of Gir | * | 5.00 | 5.00 | 11 | - | 8.0000 | Structural or unkn 💌 | 4.0000 | |
| | | Bottom of Gir | * | 1.00 | 1.00 | 11 | - | 12.0000 | Structural or unkn 💌 | 4.0000 | |
| | | Bottom of Gir | * | 2.00 | 2.00 | 11 | * | 56.0000 | Structural or unkn 💌 | 16.0000 | |
| <pre> Distance from bottom of beam </pre> | | Bottom of Gir | * | 2.00 | 2.00 | 11 | * | 70.0000 | Structural or unkn 💌 | 8.0000 | |
| | | Top of Girder | * | 2.00 | 2.00 | 4 | * | 4.0000 | Structural or unkn 💌 | 8.0000 | |
| | | | | | | | | | | | |

| e: 20% Typ | Reinforced Concrete I | | | |
|---|-----------------------|--|--|---|
| mensions Reinforcement | | | | |
| ributary width: 24.0000 in 33 | .3750 in | Top flange Material: Modular ratio: | Concrete-1922 | ~ |
| 16.0000 in 16.0000 in 16.0000 in ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ | 86.7500 in | Eff. width (Std): Eff. width (LRFD): Struct. thick.: | 24.0000 in 24.0000 in 30.0000 in | |
| 24.0000 in B: | .0000 in | | oncrete-1922 2.0 | > |
| | | | | |
| | | | | |



| - Distance from top of beam | Row | | Std bar count | LRFD bar count | Bar size | Distance (in) | Material | Bar spacing (in) | |
|---------------------------------|---------------|---|------------------|-------------------|----------|------------------|----------------------|---------------------|---|
| | Bottom of Gir | * | 5.00 | 5.00 | 11 - | 4.0000 | Structural or unkn 💌 | 4.0000 | 4 |
| | Bottom of Gir | * | 5.00 | 5.00 | 11 * | 8.0000 | Structural or unkn 💌 | 4.0000 | |
| | Bottom of Gir | - | 1.00 | 1.00 | 11 * | 12.0000 | Structural or unkn 💌 | 4.0000 | |
| | Bottom of Gir | * | 2.00 | 2.00 | 11 * | 12.0000 | Structural or unkn 💌 | 16.0000 | |
| Distance from bottom of beam | Bottom of Gir | • | 2.00 | 2.00 | 11 * | 44.0000 | Structural or unkn 💌 | 8.0000 | |
| | Top of Girder | * | 2.00 | 2.00 | 4 * | 4.0000 | Structural or unkn 💌 | 8.0000 | |
| | | | | | | | | | |

A Cross Sections

| ributary width: 24,0000 in 30,0000 in 16,0000 in 10,000 in 10,00 | Top flange Material: Concrete-1922 Modular ratio: 12.0 Eff. width (Std): 24.0000 in Eff. width (LRFD): 24.0000 in Struct. thick.: 30.0000 in |
|--|--|
| 24.0000 in B: 0.000 in in | Material: Concrete-1922 Modular ratio: 12.0 |





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| Name: 30% Dimensions Reinforcement | | Type: R | lein | forced Conc | rete l | | | | | | |
|---|---|---------------|------|------------------|-------------------|-----|------|------------------|----------------------|---------------------|------|
| ↓ Distance from top of beam ↑ • • • • • • • • • • • • • • • • • • | | Row | | Std bar count | LRFD bar count | Bar | size | Distance (in) | Material | Bar spacing (in) | |
| | Þ | Bottom of Gir | Ŧ | 5.00 | 5.00 | 11 | * | 4.0000 | Structural or unkn 💌 | 4.0000 | - |
| | | Bottom of Gir | * | 5.00 | 5.00 | 11 | Ŧ | 8.0000 | Structural or unkn 👻 | 4.0000 | |
| | | Bottom of Gir | - | 5.00 | 5.00 | 11 | Ŧ | 12.0000 | Structural or unkn 👻 | 4.0000 | |
| ⊥ ↓ Distance from bottom of beam | | Top of Girder | * | 2.00 | 2.00 | 4 | * | 4.0000 | Structural or unkn 👻 | 8.0000 | |
| | | | | | | | | | | | 4 |
| | | | | | | | | | New Duplicate | Delete | |
| | | | | | | | | | ОК Арр | ly Ca | ncel |

A Cross Sections

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| Tributary width: 24.0000 in 30.0000 in Material: Concrete-1922 |
|--|
| 16.0000 in 8. 0.0000 in B: 0.0000 in |



| ne: 40% | Type: Rein | forced Conc | rete l | | | | |
|---|-------------------|------------------|-------------------|----------|------------------|----------------------|---------------------|
| Distance from top of beam | Row | Std bar count | LRFD bar count | Bar size | Distance (in) | Material | Bar spacing (in) |
| | I Bottom of Gir * | 5.00 | 5.00 | 11 * | 4.0000 | Structural or unkn 🔻 | 4.0000 ^ |
| | Bottom of Gir 🔻 | 5.00 | 5.00 | 11 - | 8.0000 | Structural or unkn 👻 | 4.0000 |
| | Bottom of Gir 👻 | 5.00 | 5.00 | 11 * | 12.0000 | Structural or unkn 👻 | 4.0000 |
| ↓ ↓ Distance from bottom of beam | Top of Girder * | 2.00 | 2.00 | 4 - | 4.0000 | Structural or unkn 👻 | 8.0000 |
| | | | | | | New Duplicate | Delete |
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A Cross Sections

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| Name: 50% | Type: | Reinforced Concrete I | |
|---|---------|---|--|
| Dimensions Reinforcement | | | |
| Tributary width: 24.0000 in 16.0000 in 16.0000 in 24.0000 in A: 0.0000 in | - 37.00 | 000 in M Ef 05.0000 in Ef 000 in M | Concrete-1922 ✓ 12.0 24.0000 in 30.0000 in Concrete-1922 ✓ 12.0 |
| | | | OK Apply Cancel |



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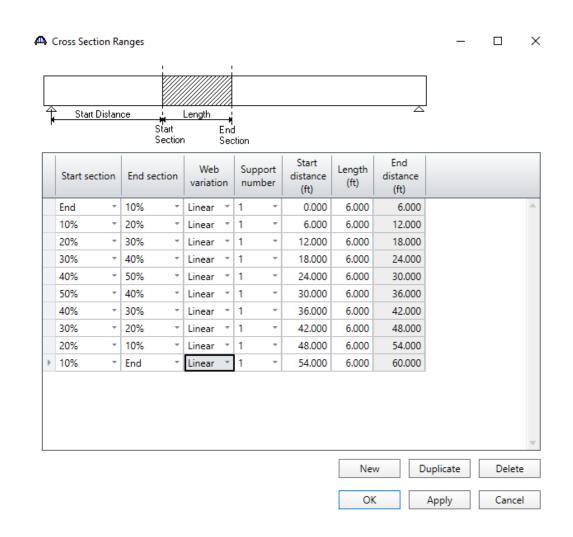
| Bottom of Gir Bottom of Gir Bottom of Gir | * * | 5.00 | 5.00 | 11 - | 4 00000 | | | |
|---|--------|------|------|----------|---------|----------------------|--------|---|
| | - | | | <u> </u> | 4.0000 | Structural or unkn 🔻 | 4.0000 | 4 |
| Bottom of Gir | | 5.00 | 5.00 | 11 * | 8.0000 | Structural or unkn 💌 | 4.0000 | |
| bottom of on | * | 5.00 | 5.00 | 11 * | 12.0000 | Structural or unkn 👻 | 4.0000 | |
| Top of Girder | - | 2.00 | 2.00 | 4 - | 4.0000 | Structural or unkn 💌 | 8.0000 | |
| | | | | | | | | |
| | | | | | | | | |





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Now that the cross sections have been entered we must assign them to the appropriate locations along the beam. Open the **Cross Section Ranges** window. The cross sections were identified for the end of the beam and then every 6 feet along the bridge length (10th points). Starting with the end of the beam select the start and end cross sections and then corresponding length between these sections. This model can be further refined with more cross section descriptions and shorter length between cross sections.







Open the **Shear Reinforcement Ranges** window and define the location and spacing of shear reinforcement as determined from the plans.

RC Shear Reinforcement Ranges



| | Name | | Support number | Start distance (ft) | Number of spaces | Spacing (in) | Length (ft) | End distance (ft) |
|---|---------------|---|-------------------|---------------------------|------------------|-----------------|----------------|-------------------------|
| s | hear stirrups | Ŧ | 1 * | 2.33 | 1 | 0.0000 | 0.00 | 2.33 |
| s | hear stirrups | Ŧ | 1 * | 2.33 | 6 | 8.0000 | 4.00 | 6.33 |
| s | hear stirrups | Ŧ | 1 * | 6.33 | 5 | 10.0000 | 4.17 | 10.50 |
| s | hear stirrups | * | 1 - | 10.49 | 6 | 12.0000 | 6.00 | 16.49 |
| s | hear stirrups | * | 1 - | 16.49 | 3 | 36.0000 | 9.00 | 25.49 |
| s | hear stirrups | * | 1 - | 20.99 | 3 | 30.0000 | 7.50 | 28.49 |
| s | hear stirrups | * | 1 - | 28.49 | 1 | 36.0000 | 3.00 | 31.49 |
| s | hear stirrups | * | 1 - | 31.49 | 3 | 30.0000 | 7.50 | 38.99 |
| s | hear stirrups | * | 1 - | 38.99 | 3 | 18.0000 | 4.50 | 43.49 |
| s | hear stirrups | * | 1 - | 43.49 | 6 | 12.0000 | 6.00 | 49.49 |
| s | hear stirrups | * | 1 - | 49.49 | 5 | 10.0000 | 4.17 | 53.66 |
| s | hear stirrups | * | 1 * | 53.66 | 6 | 8.0000 | 4.00 | 57.66 |

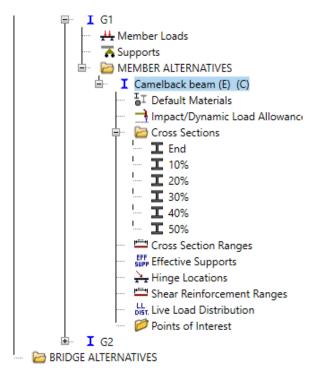
OK

Apply

Cancel



Next, copy G1 to G2. Do this by right clicking on *camelback beam (E)(C)*, select copy, then right click on **MEMBER ALTERNATIVES** under G2 and select paste.



Now that all beams within the span have been defined we are able to go back to windows within the bridge tree that will require updating.

The Live Load Distribution window for both G1 and G2 needs to be updated, select Compute from Typical Section.





🗛 Live Load Distribution

| | ndard LRF | | | | | |
|---|--------------------------------|-----------|-------------------|-------------------------|----------------|---|
| | Distribution fa | | | | | |
| (| Use simpli | fied met | hod 🔾 | Use advanc | ed method | ○ Use advanced method with 1994 guide specs |
| | Allow distrib | ution fac | tors to be u | used to com | pute effects o | of permit loads with routine traffic |
| | Lanes | | | ution factor /heels) | | |
| | loaded | Shear | Shear at supports | Moment | Deflection | |
| Þ | 1 Lane | 1.500 | 1.500 | 1.500 | 1.000 | 1 |
| | Multi-lane | 2.083 | 2.083 | 2.083 | 2.000 | |
| | | | | | | |
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| - | | | | | | |
| | Compute from ypical section | | View calcs | | | |
| | | | View calcs | | | |

Bridge Alternatives

Now that the superstructure definitions are modeled, Bridge Alternatives must be created. This makes it possible to rate the entire bridge at one time and also perform batch processes in the Bridge Explorer workspace, which is important for permitting issues.

For load rating, there will typically be only one Bridge Alternative. Another Bridge Alternative could be created for a proposed bridge or rehabilitation project, but only one bridge alternative should be existing/current at a time. Each superstructure that was entered above now needs its own definition in the Bridge Alternative. Select the superstructure wizard. Enter the number of superstructures. Enter the superstructure and





superstructure alternative names and then select the superstructure definition that you want to link to each alternative.

The bridge alternative portion of the tree may be created manually by double-clicking on each branch and assigning the necessary bridge components to each branch as shown above (**Superstructure Wizard...** button may be selected to aid in this process). Double-click **BRIDGE ALTERNATIVES** and enter the Alternative Name, then select the **Superstructure Wizard...** button and enter the data shown in the window below.

| 🗛 Superstructu | re Wizard | | | | × |
|----------------------|----------------------|--|---------------------------|---------------|---------|
| Definitions to the | e new alternativ | Superstructures, Superstruct res. The wizard will also creat Bridge Alternative does not c | e Piers if you are r | unning BrD Su | |
| Number of super | rstructures | 1 | | | |
| Prefix to use w | hen generating | names | | | |
| Superstructure | e prefix: | Superstructure % | Gene | rate names | |
| Superstructur | e alternative pro | efix: Superstructure Alt % | Gene | rate names | |
| Superstructu name | ure Distance (ft) | Superstructure alternative name | Superstructure definition | | |
| I Camelback | | Camelback | Camelback - | | |
| | | | | | * |
| Substructure u | nits | | | | |
| First unit type: | Abutment | ~ | | | |
| Last unit type: | Abutment | ~ | | | |
| | | | | | |

Click **Finish** to close the Superstructure Wizard and **OK** to save the Bridge Alternative data to memory and close the window.





Analysis

Vehicle Selection

From the *Bridge* menu, select *Analysis Settings* and load the following vehicles into the rating column:

| Design review Rating Rating method: LFD Image: Comparison of the second of the | 🕰 Analysis Settings | | _ | | > |
|--|---|--|----------|-------|----|
| Lane / Impact loading type: As Requested Apply preference setting: None Add to Add to Add to Add to Add to Add to Add to Add to Add to Add to Add to Add to Add to Add to Add to A | O Design review Rating | Rating method: LFD | ~ | | |
| Vehicles Output Engine Description Traffic direction: Both directions Refresh Temporary vehicles Advanced Vehicle selection Vehicle summary Michigan 2 Unit Truck 13-NL Michigan 2 Unit Truck 15-DL Michigan 2 Unit Truck 15-NL Michigan 2 Unit Truck 16-NL Michigan 2 Unit Truck 18-NL Michigan 2 Unit Truck 18-NL Michigan 3 Unit Truck 20-NL Michigan 3 Unit Truck 20-NL Michigan 3 Unit Truck 21-NL Michigan 3 Unit Truck 22-NL Michigan Overload Truck 03 Class A Michigan Overload Truck 03 Class A<td>Analysis type: Line Girder</td><td>V</td><td></td><td></td><td></td> | Analysis type: Line Girder | V | | | |
| Traffic direction: Both directions Refresh Temporary vehicles Advanced Vehicle selection Vehicle summary Immentance Immentance Immentance Immentance Michigan 2 Unit Truck 13-NL Michigan 2 Unit Truck 15-NL Immentance Immentance Immentance Michigan 2 Unit Truck 15-NL Michigan 2 Unit Truck 15-NL Immentance Immentance Immentance Michigan 2 Unit Truck 15-NL Michigan 2 Unit Truck 15-NL Immentance Immentance Immentance Michigan 2 Unit Truck 15-NL Michigan 2 Unit Truck 16-NL Immentance Immentance Immentance Michigan 2 Unit Truck 18-NL Michigan 3 Unit Truck 20-DL Immentance Immentance Immentance Michigan 3 Unit Truck 20 Michigan 3 Unit Truck 21-DL Immentance Immentance Immentance Michigan 3 Unit Truck 22-NL Michigan 3 Unit Truck 22-NL Immentance Immentance Immentance Michigan 3 Unit Truck 22-NL Michigan 3 Unit Truck 22-NL Immentance Immentance Immentance Michigan 3 Unit Truck 22-NL Michigan 3 Unit Truck 22-NL Immentance Immentance Immentance Michigan 3 Unit Tru | Lane / Impact loading type: As Requested | Apply preference setting: None | ~ | | |
| Vehicle selection Vehicle summary -Michigan 2 Unit Truck 13-NL -Michigan 2 Unit Truck 15-DL -Michigan 2 Unit Truck 15-NL -Michigan 2 Unit Truck 15-NL -Michigan 2 Unit Truck 16-DL -Michigan 2 Unit Truck 16-DL -Michigan 2 Unit Truck 17-DL -Michigan 1 Unit Truck 05-DL -Michigan 2 Unit Truck 18-DL -Michigan 1 Unit Truck 05-DL -Michigan 2 Unit Truck 18-DL -Michigan 3 Unit Truck 23-DL -Michigan 3 Unit Truck 19-DL -Michigan 3 Unit Truck 22-DL -Michigan 3 Unit Truck 21-DL Remove from -Michigan 3 Unit Truck 22-DL -Michigan 3 Unit Truck 22-NL -Michigan 3 Unit Truck 22-NL <t< td=""><td>Vehicles Output Engine Description</td><td></td><td></td><td></td><td></td></t<> | Vehicles Output Engine Description | | | | |
| Michigan 2 Unit Truck 13-NL Michigan 2 Unit Truck 15-DL Michigan 2 Unit Truck 15-DL Michigan 2 Unit Truck 16-DL Michigan 2 Unit Truck 16-DL Michigan 2 Unit Truck 17-DL Michigan 2 Unit Truck 17-DL Michigan 2 Unit Truck 18-DL Michigan 2 Unit Truck 18-DL Michigan 3 Unit Truck 19-DL Michigan 3 Unit Truck 20 Michigan 3 Unit Truck 21-DL Michigan 3 Unit Truck 22-DL Michigan 3 Unit Truck 05-DL Michigan 3 Unit Truck 05-DL Michigan 3 Unit Truck 05-DL Michigan 4 Unit Truck 05-DL Michigan 0 Verload Truck 05 Class A Michigan 0 Verload Truck 03 Class A | Traffic direction: Both directions | Refresh Temporary vehicles | Advanced |] | |
| Michigan 2 Unit Truck 14 Michigan 2 Unit Truck 15-DL Michigan 2 Unit Truck 15-NL Michigan 2 Unit Truck 16-DL Michigan 2 Unit Truck 16-NL Michigan 2 Unit Truck 17-DL Michigan 2 Unit Truck 18-NL Michigan 2 Unit Truck 18-DL Michigan 2 Unit Truck 18-DL Michigan 3 Unit Truck 19-DL Michigan 3 Unit Truck 20 Michigan 3 Unit Truck 21-DL Michigan 3 Unit Truck 22-DL Michigan 3 Unit Truck 22-NL Michigan 3 Unit Truck 23-DL Michigan 3 Unit Truck 22-NL Michigan 3 Unit Truck 23-DL Michigan 3 Unit Truck 23-DL Michigan 3 Unit Truck 22-NL Michigan 3 Unit Truck 23-DL Michigan 4 Unit Truck 23-DL Michigan 5 Unit Truck 23-DL Michigan 6 Unit Truck 23-DL Michigan 7 Unit Truck 25-DL Michigan | Vehicle selection | Vehicle summary | | | |
| Michigan Overload Truck 05 Class AMichigan Overload Truck 06 Class A | Michigan 2 Unit Truck 14 Michigan 2 Unit Truck 15-DL Michigan 2 Unit Truck 15-NL Michigan 2 Unit Truck 16-DL Michigan 2 Unit Truck 16-NL Michigan 2 Unit Truck 17-DL Michigan 2 Unit Truck 17-NL Michigan 2 Unit Truck 18-DL Michigan 2 Unit Truck 18-DL Michigan 3 Unit Truck 19-DL Michigan 3 Unit Truck 19-NL Michigan 3 Unit Truck 21-DL Michigan 3 Unit Truck 21-DL Michigan 3 Unit Truck 22-DL Michigan 3 Unit Truck 23-DL Michigan 3 Unit Truck 23-DL Michigan 3 Unit Truck 24-DL Michigan 3 Unit Truck 24-DL Michigan 3 Unit Truck 25-DL Michigan 0verload Truck 02 Class A Michigan Overload Truck 04 Class A Michigan Overload Truck 04 Class A Michigan Overload Truck 05 Class A | Add to Ad | | | |
| Reset Clear Open template Save template OK Apply Cancel | Reset Clear Open template | ave template OK | Apply | Cance | el |

Select **OK**

Note: MDOT trucks 5-DL, 18-DL and 23-DL are used in this analysis as they are the commonly controlling 1-unit, 2-unit and 3-unit trucks, respectively. The load rating engineer should evaluate the list of legal vehicles to determine whether others may control and include them in the analysis if necessary. In addition, if posting is required, all legal loads must be analyzed to determine the lowest tonnage for each vehicle category.





Analysis

Go to *Bridge/Analyze*. You will be informed regarding progress and completion of the analysis.

| Analysis Progress | |] |
|-------------------|--|----|
| Analysis Event | Location - 6.0000 (ft) Location - 12.0000 (ft) Location - 18.0000 (ft) Location - 24.0000 (ft) Location - 30.0000 (ft) Location - 36.0000 (ft) Location - 42.0000 (ft) Location - 48.0000 (ft) Location - 54.0000 (ft) Location - 54.0000 (ft) Location - 60.0000 (ft) Location - 5.9545 (ft) Location - 53.9934 (ft) Completed Specification Check. Info - Finished LFR specification checking Info - Finished populating specification checking results Info - Analysis completed! | E |
| ۰ III ا | < | F |
| View Rating Log | Print | ОК |

Reporting

Results of the analysis may be viewed using the *Report Tool* located within the *Bridge* menu.

| A Camelback | - LFD Report | - • • |
|--|--|-------------------------------|
| Report Type: | LFD Analysis Output Advanced Begin each topi | ic on a new page when printed |
| Report New | Open Merge Save Save As | Generate |
| ☐ Reactions ☐ Moments ☐ Shears ☐ Cross Sect | Vehicle Rating Summary tion Properties ating Results | |
| Clear All | Select All Delete | Close |

Select Generate.





Bridge Name: Sample of a Camelback Bridge Load Rating NBI Structure ID: camelback1 Bridge ID: camelback1

Analyzed By: BrR Analyze Date: Monday, September 13, 2016 12:58:35 Analysis Engine: AASHTO LFR Engine Version 7.0.3001 Analysis Preference Setting: None

Report By: brr Report Date: Monday, September 13, 2021 13:00:09

Structure Definition Name: camelback Member Name: G1 Member Alternative Name: camelback beam

| | | | Load Factor | Rating Summ | nary | | | | |
|--------------------------------|-----------|--------|-------------------------|-------------|------|---------------|---------|--------------|--------------|
| | | Rating | | Capacity | | Location | | | |
| Live Load | | Factor | Controls | (Ton) | Span | (ft) | Percent | Impact | Lane |
| HS 20-44 | Inventory | 0.836 | Design Shear - Concrete | 30.11 | 1 | 60.00 | 100.0 | As Requested | As Requested |
| HS 20-44 | Operating | 1.397 | Design Shear - Concrete | 50.28 | 1 | 60.00 | 100.0 | As Requested | As Requested |
| Michigan 1 Unit Truck 05-DL | Operating | 1.334 | Design Shear - Concrete | 56.04 | 1 | 60.00 | 100.0 | As Requested | As Requested |
| Michigan 2 Unit Truck 18-DL | Operating | 0.901 | Design Shear - Concrete | 69.38 | 1 | 60.00 | 100.0 | As Requested | As Requested |
| Michigan 3 Unit Truck 23-DL | Operating | 0.962 | Design Shear - Concrete | 74.10 | 1 | 60.00 | 100.0 | As Requested | As Requested |

Note: "N/A" indicates not applicable "**" indicates not available





Bridge Name: Sample of a Camelback Bridge Load Rating NBI Structure ID: camelback1 Bridge ID: camelback1

Analyzed By: BrR Analyze Date: Monday, September 13, 2016 12:58:35 Analysis Engine: AASHTO LFR Engine Version 7.0.3001 Analysis Preference Setting: None

Report By: brr Report Date: Monday, September 13, 2021 13:00:09

Structure Definition Name: camelback **Member Name:** G2 **Member Alternative Name:** Copy of camelback beam

Load Factor Rating Summary

| | | Rating | | Capacity | | Location | | | |
|--------------------------------|-----------|--------|-------------------------|----------|------|---------------|---------|--------------|--------------|
| Live Load | | Factor | Controls | (Ton) | Span | (ft) | Percent | Impact | Lane |
| HS 20-44 | Inventory | 0.836 | Design Shear - Concrete | 30.11 | 1 | 60.00 | 100.0 | As Requested | As Requested |
| HS 20-44 | Operating | 1.397 | Design Shear - Concrete | 50.28 | 1 | 60.00 | 100.0 | As Requested | As Requested |
| Michigan 1 Unit Truck 05-DL | Operating | 1.334 | Design Shear - Concrete | 56.04 | 1 | 60.00 | 100.0 | As Requested | As Requested |
| Michigan 2 Unit Truck 18-DL | Operating | 0.901 | Design Shear - Concrete | 69.38 | 1 | 60.00 | 100.0 | As Requested | As Requested |
| Michigan 3 Unit Truck 23-DL | Operating | 0.962 | Design Shear - Concrete | 74.10 | 1 | 60.00 | 100.0 | As Requested | As Requested |

Note: "N/A" indicates not applicable "**" indicates not available

